

Venting the CFHT Dome



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CFHT Users' Meeting – May, 2010

Acknowledgements

IQ studies, guidance and wisdom

Rene Racine

Water / wind tunnel models and tests

Marc Baril

Tom Benedict

Karun Thanjavur

Shiang Yu Wang – ASIAA

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CFD calculations

Konstantinos Vogiatzis

Vent Project Team

Contract and mechanical hardware

Steve Bauman (Project Manager)

DeeDee Warren

CFHT daycrew

Software and controls

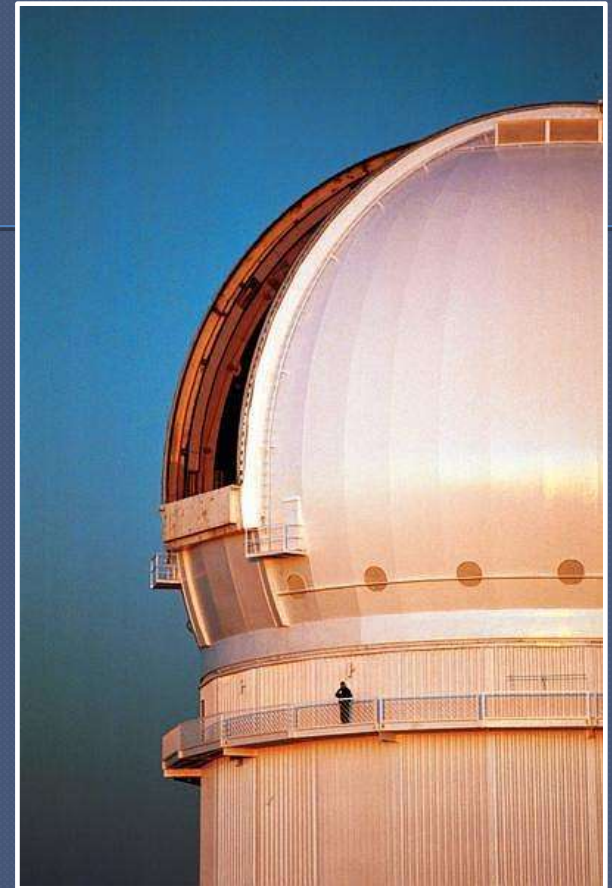
Tom Vermeulen Larry Roberts

Grant Matsushige

Fluid dynamics consultants

Bob Breidenthal – U of Washington

Bernard Tanguay – NRC-IAE Aerodynamics Lab



Contractors

- Caid Industries
- M3
- Nexus Steel
- SteelTech

Facility seeing – what causes it?

Optical turbulence (facility seeing) requires:

- physical turbulence
- incomplete mixing of air parcels of differing temperature
- transport of poorly mixed air into the optical path

Temperature of advected air changes much more rapidly than structural temperatures

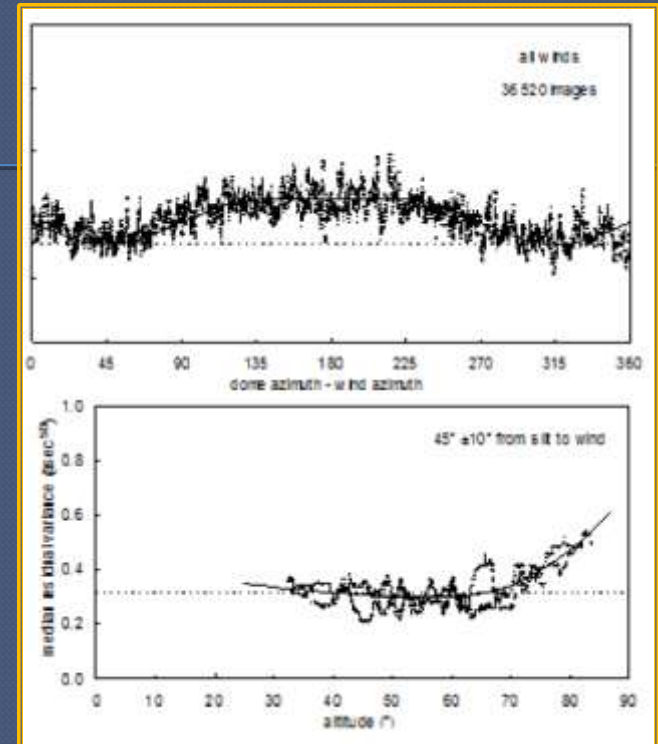
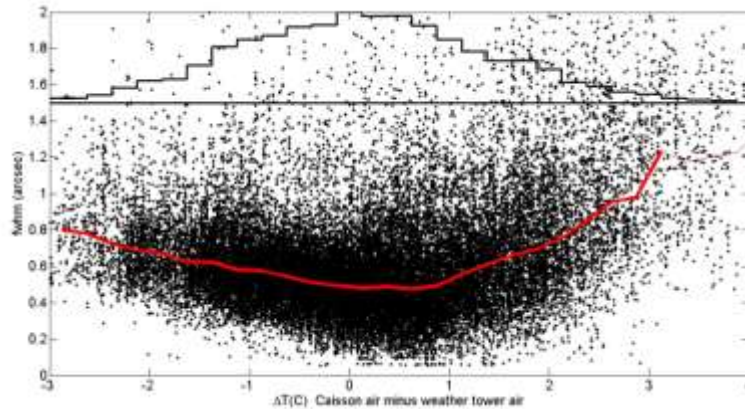
- air temperature is changed when in contact with heavy structures
- stagnant air leads to large ΔT

Two passive solutions:

- minimize ΔT between air and telescope structures (insulate) and/or
- limit the time air is in contact with structures (venting)

IQ pathologies

- image quality degrades when :
 - dome air temp differs from outside air
 - the dome slit points downwind
 - observing near the zenith

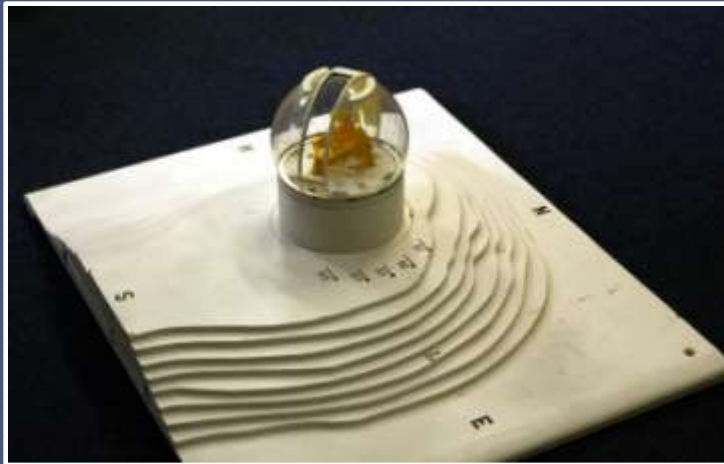


Approach to vent development

- Understand air flow in and around the dome – limits on improvements
 - Fluid dynamics consultants and literature
 - Water tunnel tests of 160:1 scale model
 - Computational fluid dynamics models
- Understand the dome structure and limitations to vent design / installation
 - Excellent set of construction drawings from Brittain Steel (DSL)
 - Computer solid model of dome and telescope
- Contract structural design firms to develop vents within budget, schedule and existing structure
 - Structural analysis of the vented dome
 - Detail and fabrication drawings
 - Fabrication
 - Installation

Flow in the dome

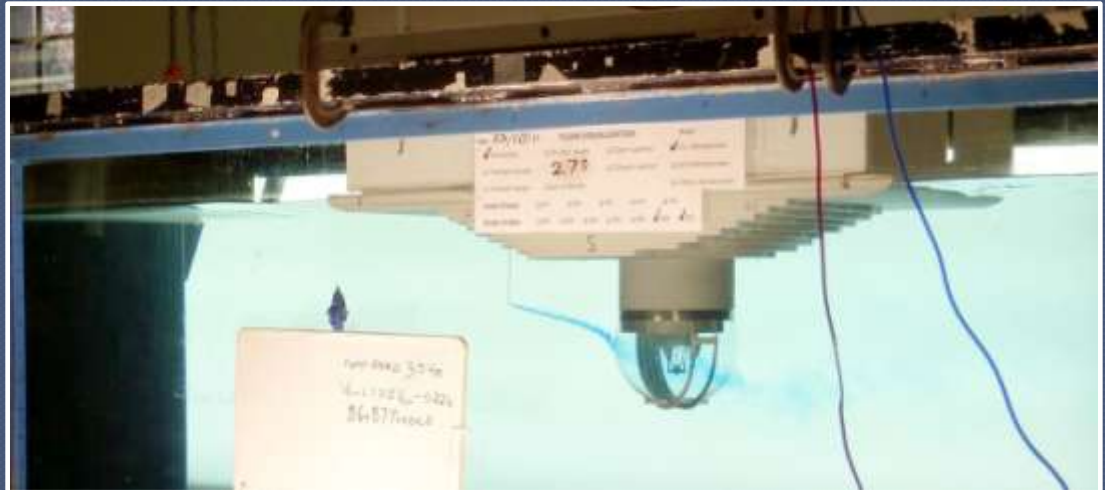
– U of Washington water tunnel



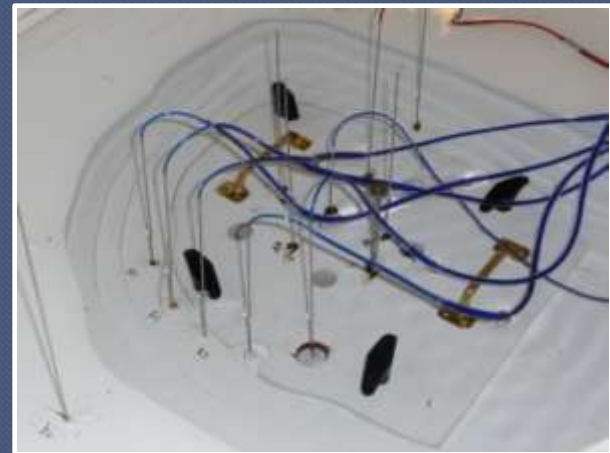
The CFHT Water Men

- Tom Benedict
- Marc Baril
- Karun Thanjavur

Water tunnel model



- terraced terrain model
- flow from the East
- full dome rotation
- dye probes
 - 6 in dome
 - 5 up stream
 - 2 down stream



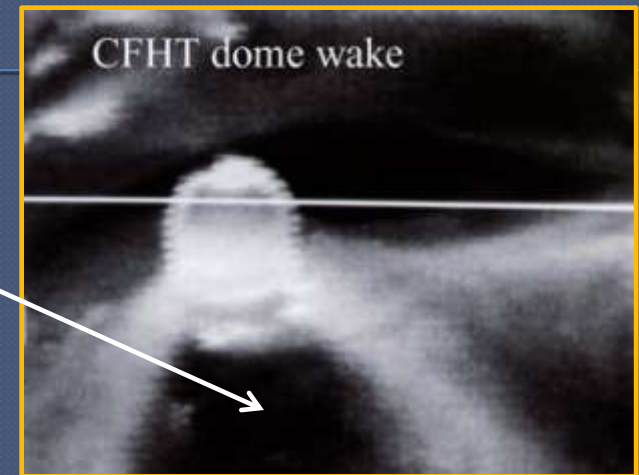
Water tunnel test suite

- Flow from east only
- All dome slit orientations: east through south to west – 15 degree increments
- Vents
 - Unvented dome
 - 8 small vents
 - 8 larger vents
- Flushing / clearing times
- Flow patterns
 - onto dome
 - in lee of dome
 - inside dome starting at floor level
 - inside dome in telescope tube

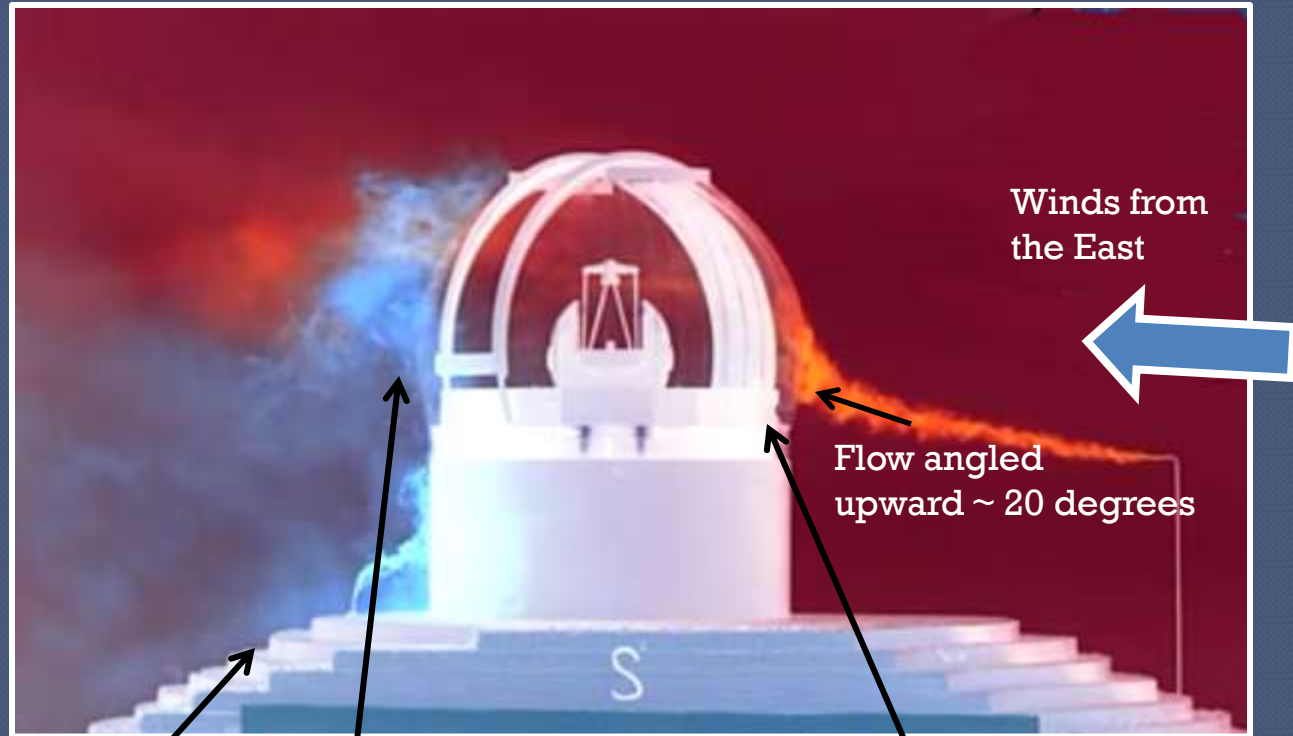
Horseshoe vortex

Vortex scours cold air and lifts it to height of building radius

Air in contact with ground
5 to 8 C below ambient



Flow around the dome - water tunnel



Winds from
the East

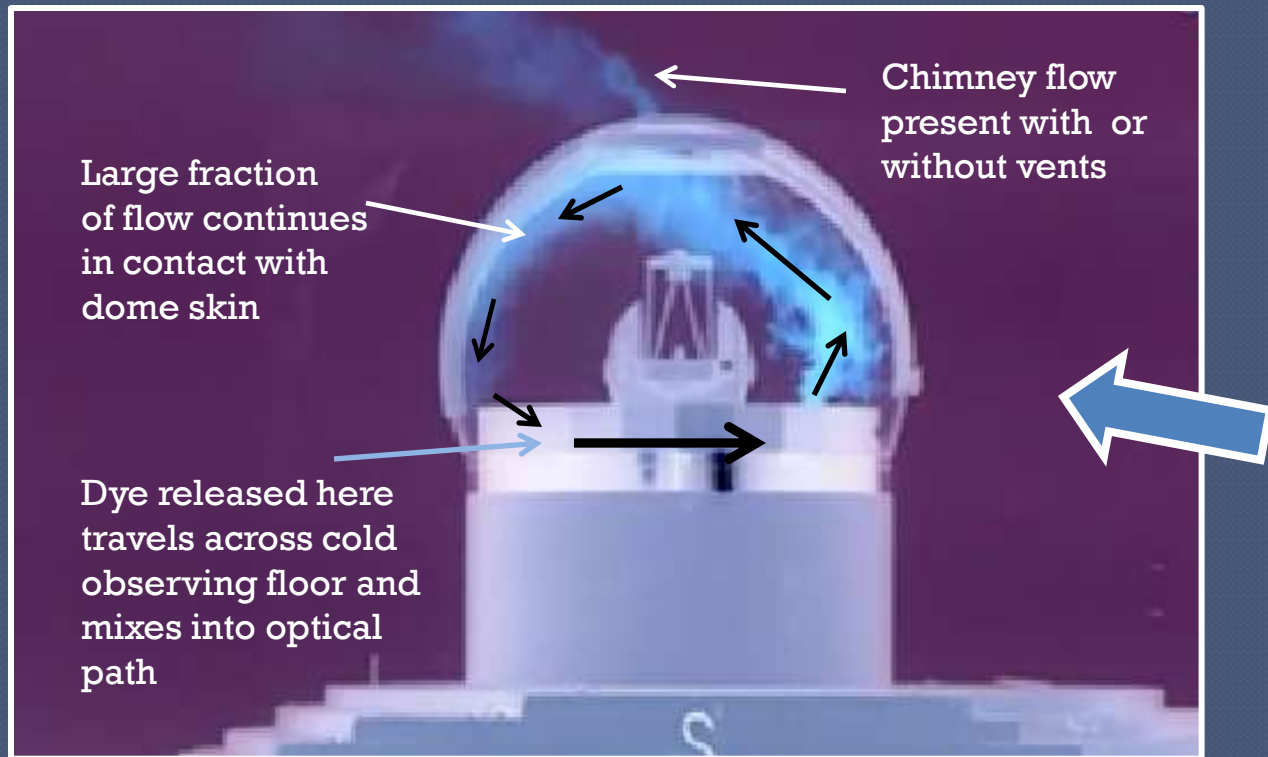
Flow angled
upward ~ 20 degrees

Lee side upwelling

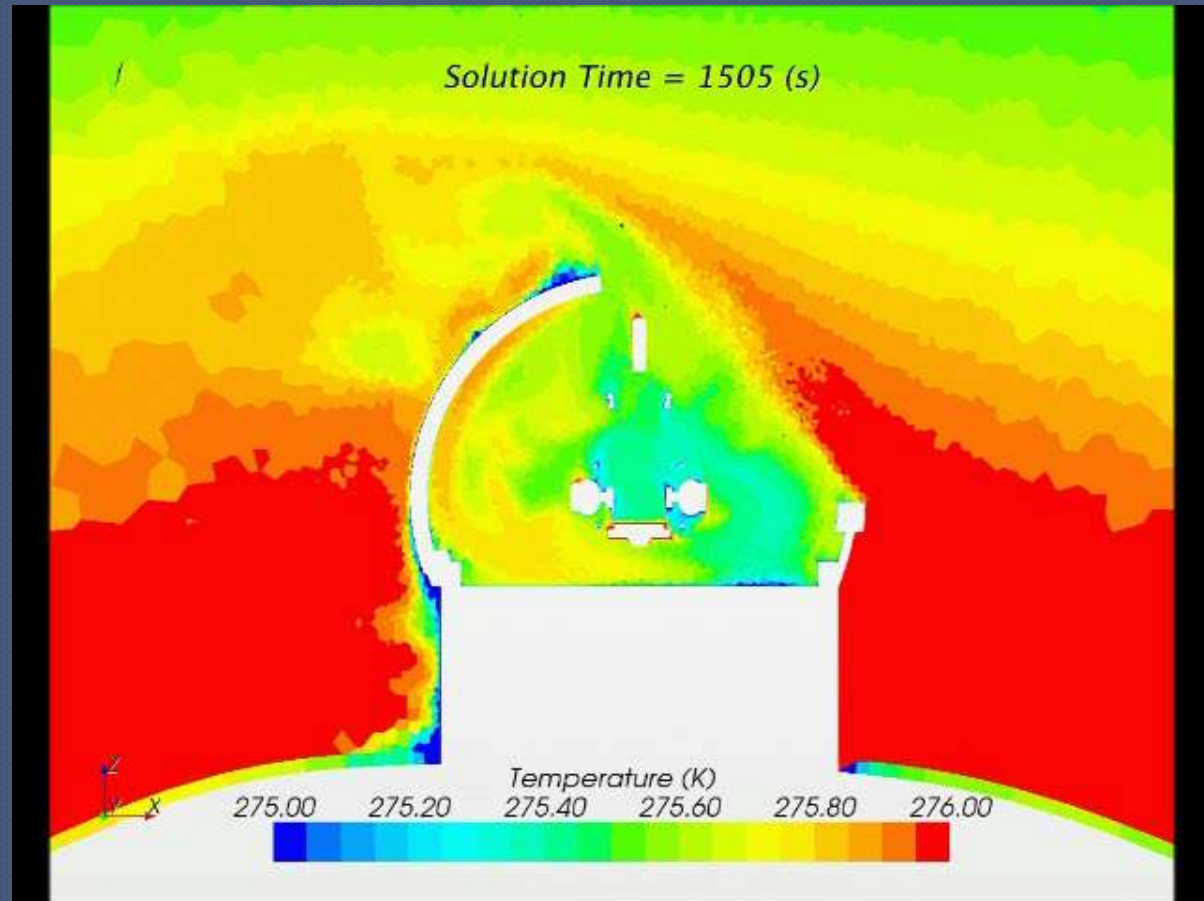
Upwind stagnation point
(best vent location) is low

Radiatively cooled
terrain

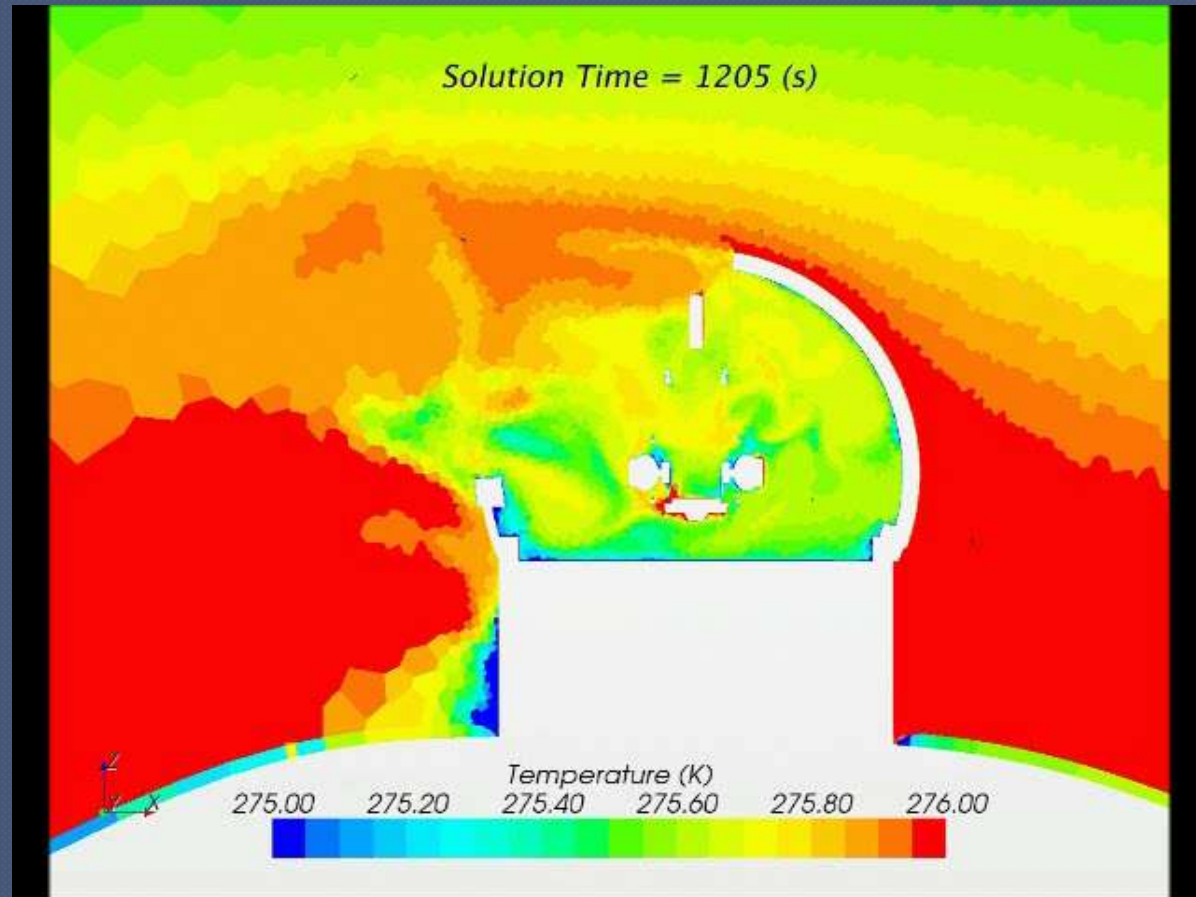
Simple flow case – slit into the wind



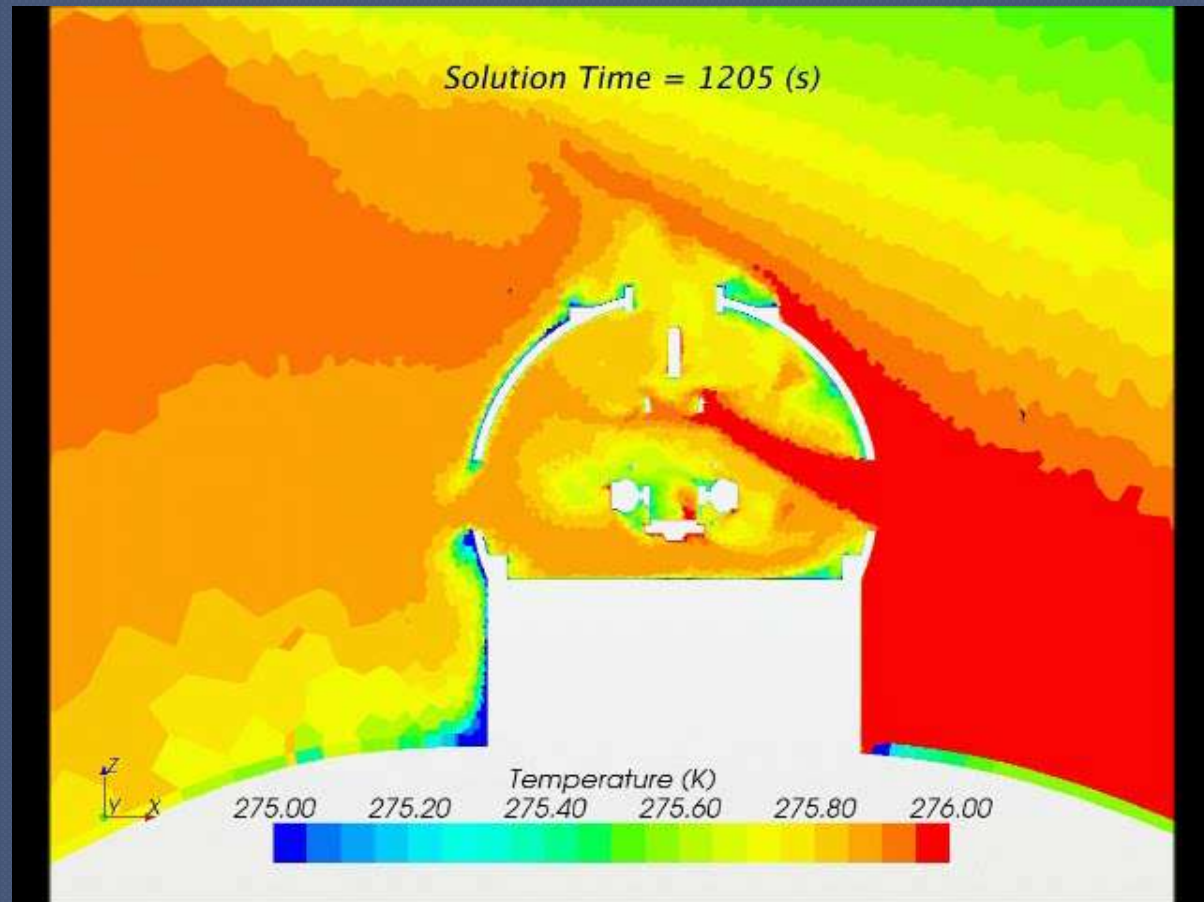
CFD : Dome Unvented – Slit Upwind



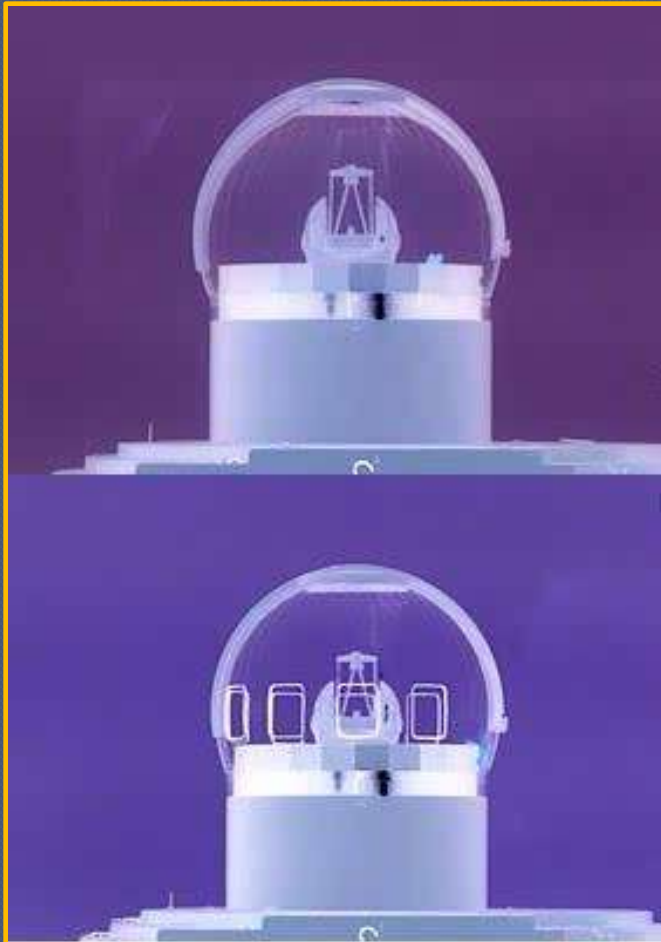
CFD – Dome unvented – Slit Downwind



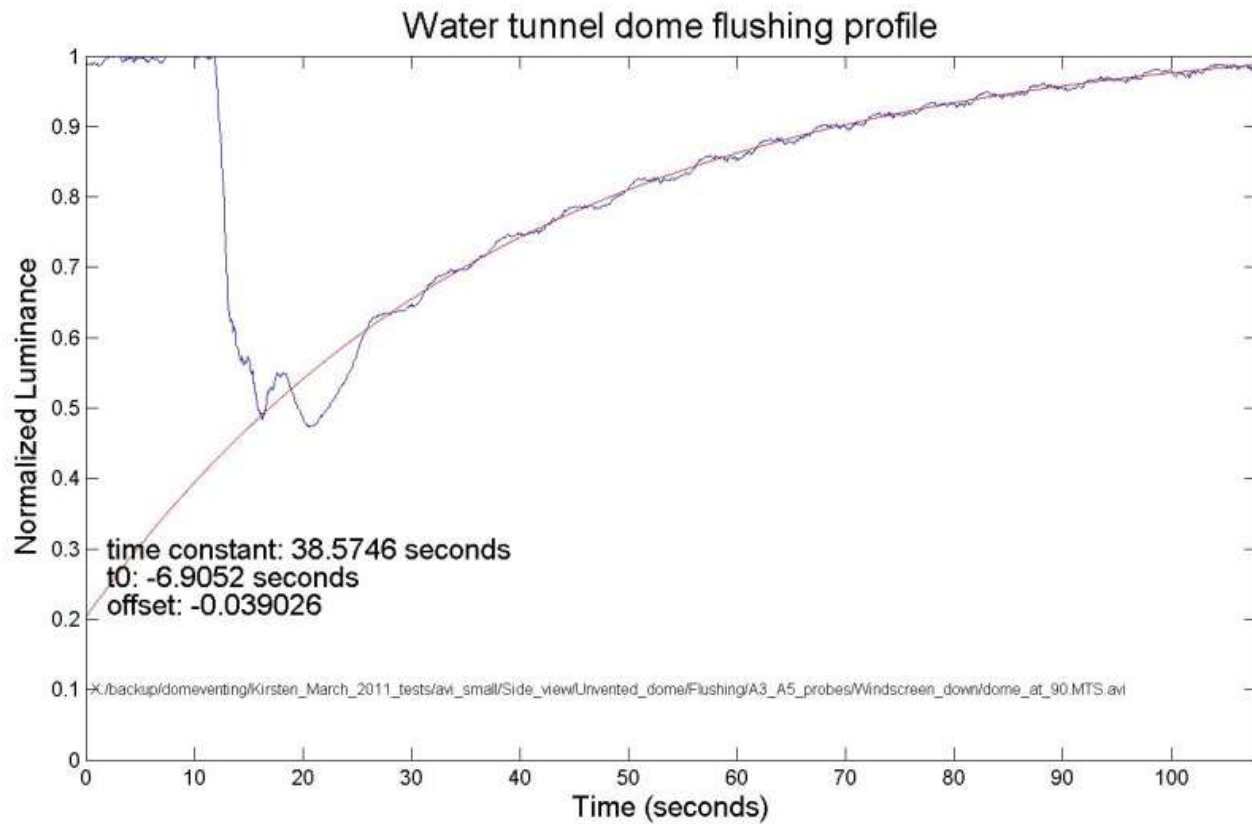
CFD - Dome Vented - Slit South



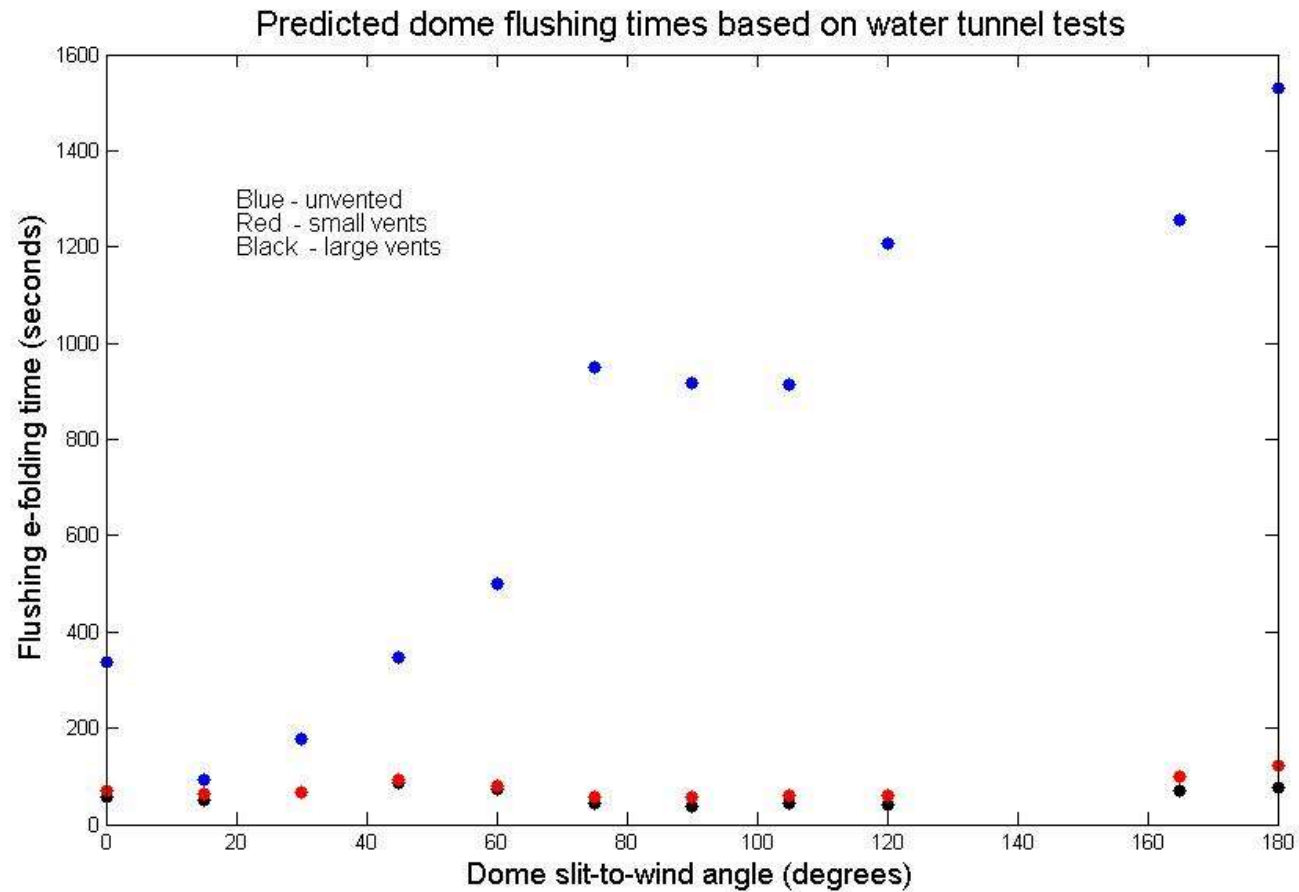
Flow visualization – a few water tunnel examples



Flush time estimates



Flush times – vented vs unvented



Study conclusions

- Closed enclosure is a bad idea
 - stagnation leads to large Δ Temp in air
 - circulation into optical path
 - mirror seeing is likely NOT the dominant contributor to facility seeing
- Venting works
 - better flushing leads to lower air Δ Temp
 - strategies needed to deal with jetting
- Chimney maintained at many slit orientations – but not all
 - Slit front and back might reduce chimney effect (a la NTT)
- Upwelling downwind should be controlled
- Upwind flow tilted upward about 20 degree (Ando and Seigmund)
 - stagnation point low on the vertical cross section
 - keep vents low for most efficient flushing
- Effective vent area \ll projection onto upstream flow
 - flow runs tangent to skin away from stagnation point
- Low level vortex – keep openings above height = building radius
 - possibility of cold ground air mixed into the dome.

Procurement milestones

Bids solicited from 8 pre-selected vendors – November, 2011

- design, build, install

4 participated in on-site pre-bid review – December, 2011

3 responses – February, 2012

- San Jaun Construction	\$3.4 M US
- B&C Southwest	\$1.9 M US
- SteelTech (M3 – CAID – Nexus)	\$1.6 M US – selected

6 month delay due to dome shutter

CRC / Board approval – October, 2012

OMKM / DLNR approval – December, 2012

Contract signed – December, 2012

Prototype installed – April, 2013

Final install – September, 2013

Design approach

Functional goals – vent should:

- wide
- low on the dome skin
- maximum possible area !

Real world constraints

- budget
- dome vertical structural webs
- dome power bus bars and inner catwalk
- mezzanine blockage
- sever summit weather

Final design:

Vendor

- 12 vents – opening 1.8 m x 5 m
- concentrated toward back side
- vertical roll-up weather door
- vane (louver) on interior face
- drive motors, position sensors, electrical interface box

CFHT

- computer (PLC) control with status log
- user interface for RO's and engineering

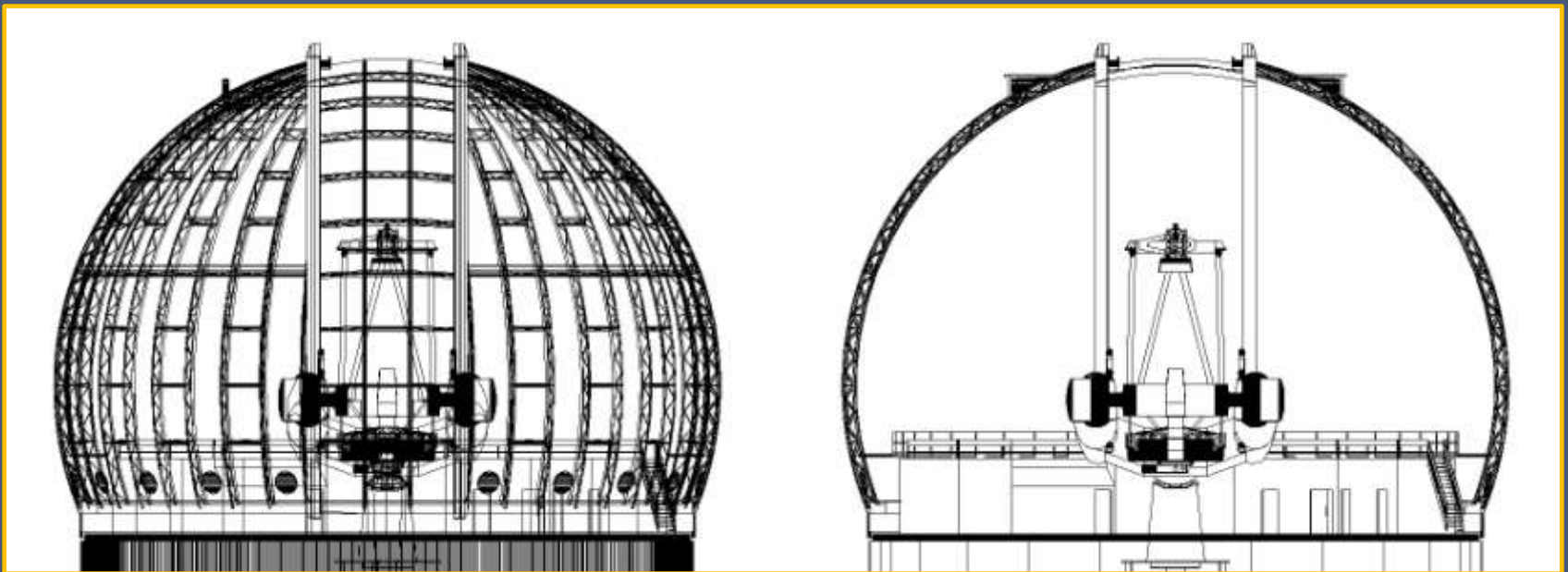
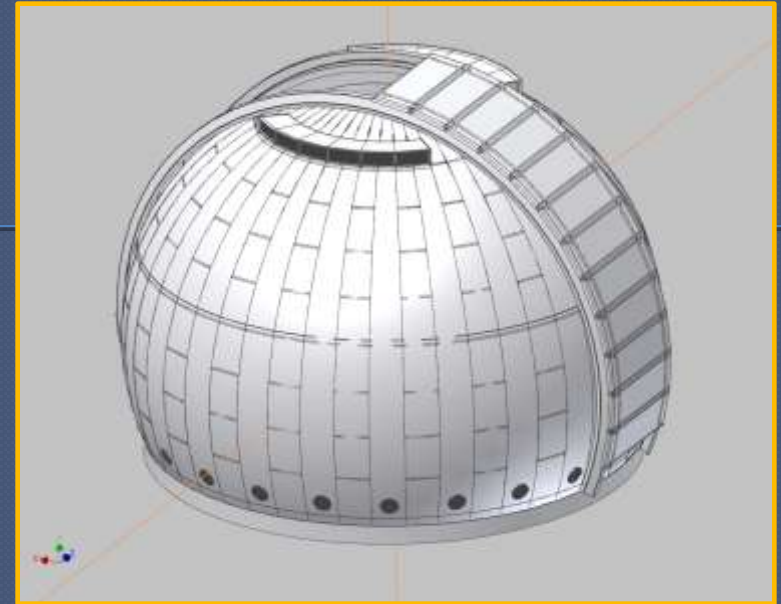


Dome structure

Vertical gores – $\frac{1}{4}$ inch steel plate

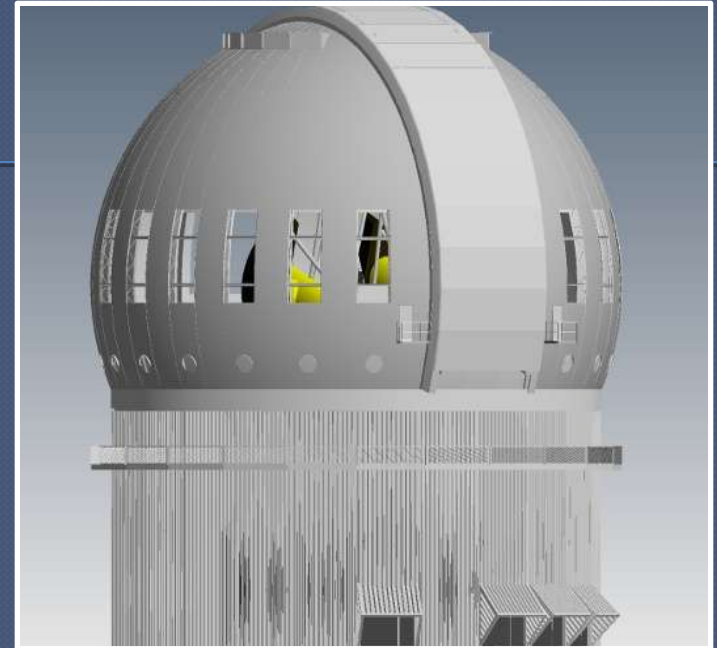
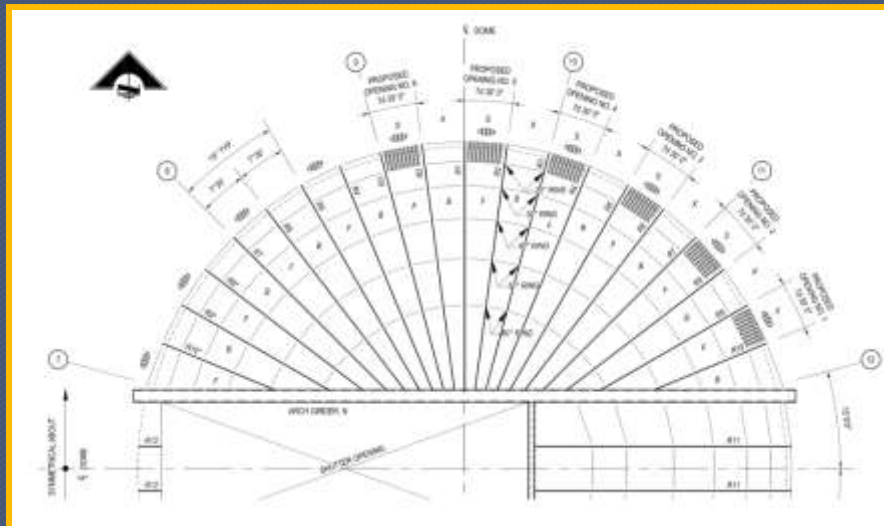
Vertical stiffening rib trusses

Horizontal trusses on alternating gores



Design outline

- 12 vent units – 6 per side – cost constrained
 - 15 degree intervals
- mounted from the outside
- no observing down time
 - work from 7:00 to 16:30



Vent units

vents delivered as assembled units

units extend from outer dome shell
to inner insulation shell

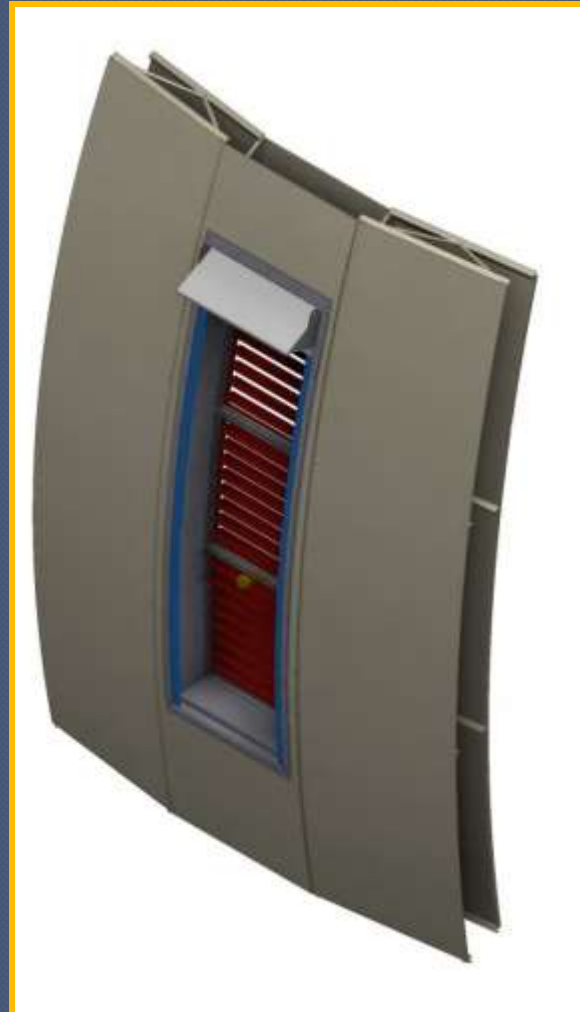
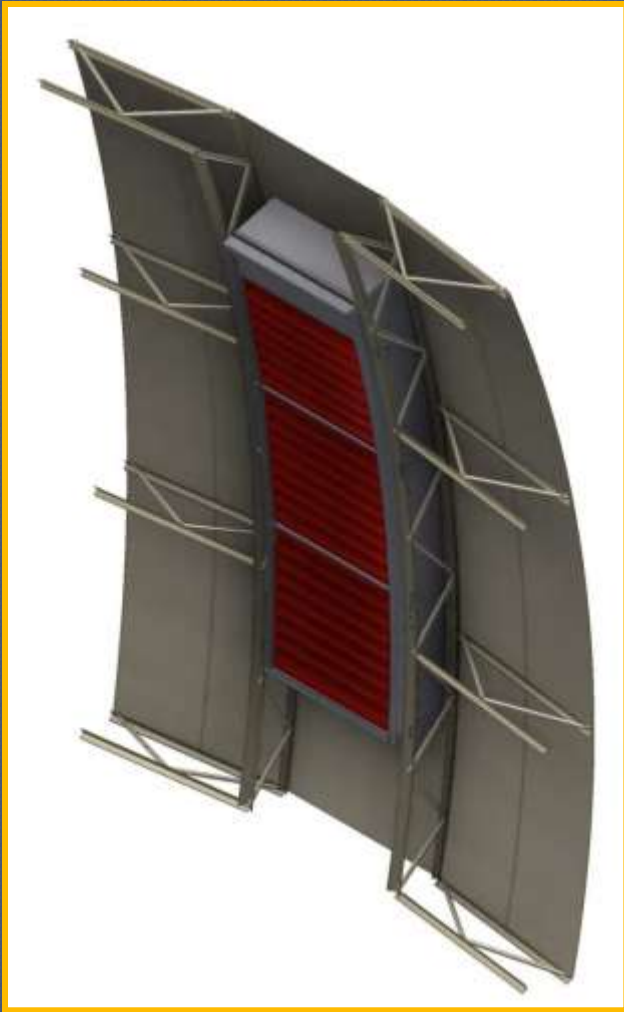
sealed from inter-skin cavity

Outer rollup 'garage' door

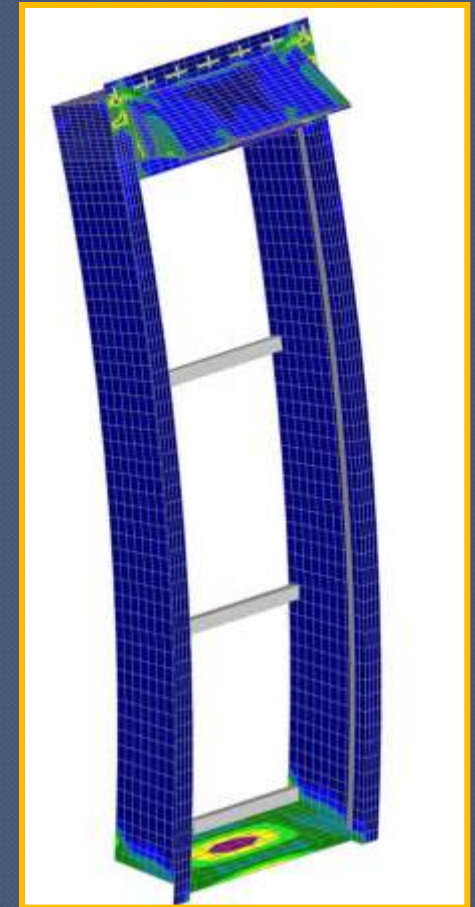
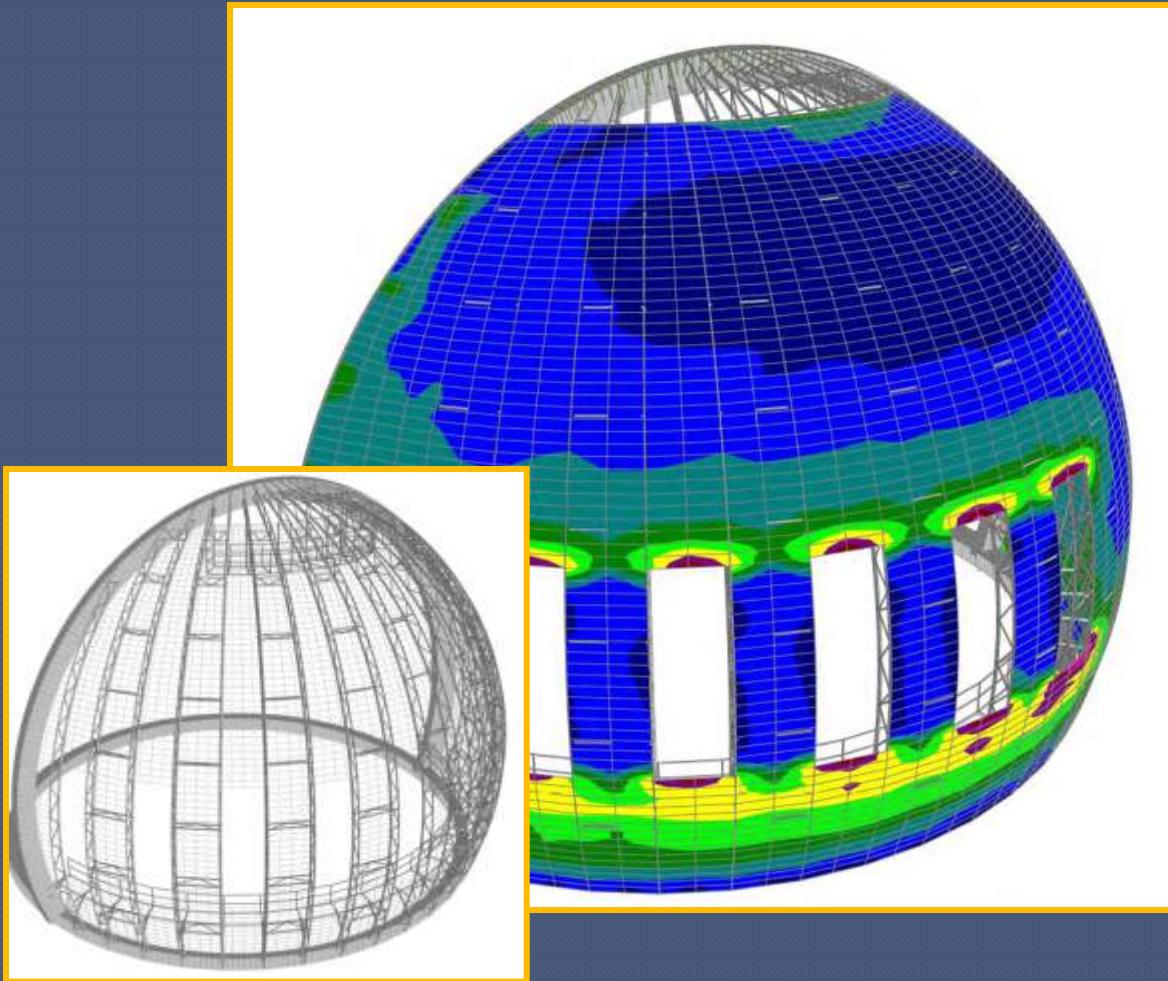
- weather doors
- flow throttling – 4 positions
 - fully open
 - 2/3 open
 - 1/3 open
 - fully closed
- inner vanes
 - flow redirection
 - flow throttling
 - weather backup
 - easily removable



Vent unit placement



Structural analysis and design – M3 Engineering



The real thing – CAID Industries



Prototype installation – April 24, 2013



Prototype installation – April 24, 2013



Prototype installation – April 24, 2013



Prototype installation – April 24, 2013



Prototype installation – April 24, 2013



Prototype installation – April 24, 2013



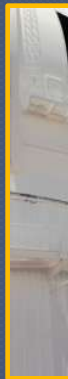
Prototype installation – April 24, 2013



Prototype installation – April 24, 2013



Prototype installation – April 24, 2013



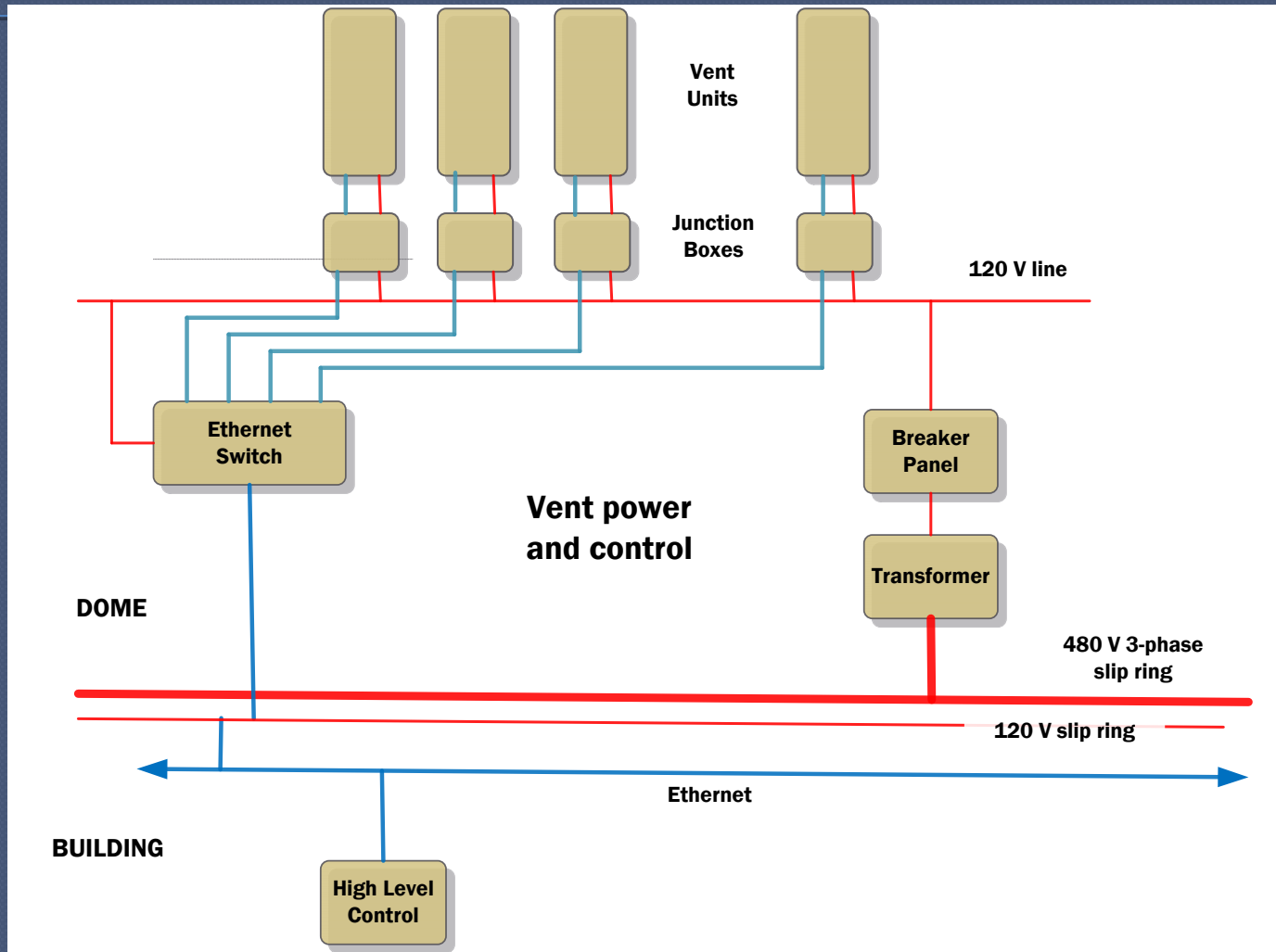
Prototype installation – April 24, 2013



Prototype – April 26, 2013



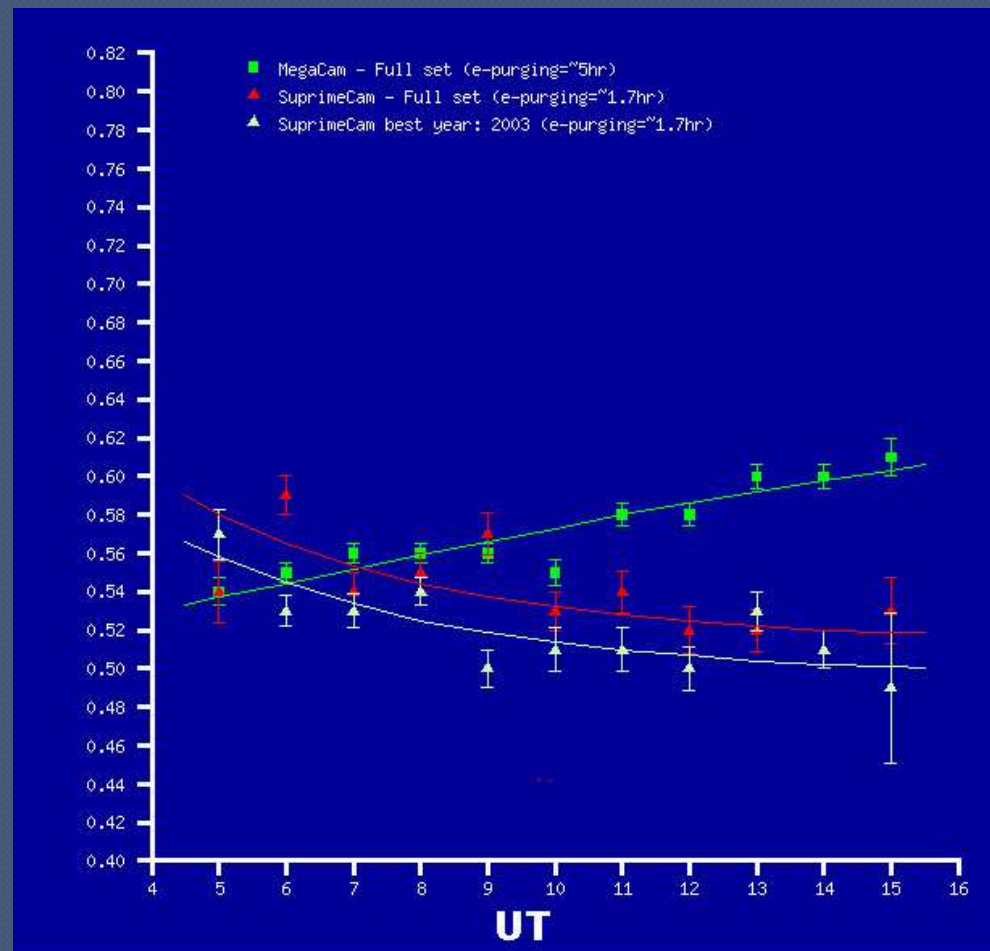
Control architecture



Controls and RO interactions

- Initially RO can select between 3 modes of operation – no “random” RO control permitted
 - Mode 1 fully closed – wind, rain, snow, daytime – whatever mode
 - Mode 2 all vents fully open, vanes pointed 20 degrees – directly into wind
 - Mode 3 vents fully open vanes 20 degree down into wind, BUT to reduce wind shake:
 - a) upwind vent(s) 1/3 closed or ...
 - b) upwind vent(s) 2/3 closed or ...
 - c) upwind vent(s) fully closed
- Reconfigure vents only if telescope is tracking (avoids crazies during slews)
- Reconfigure vents only if dome rotated more than 10 degrees

... and the gain is ?



Coming in September – 11 more !



Stay Tuned !

Primary mirror refiguring – ROM cost estimates

Requirements:

- cost / schedule for in-house work only (exclusive of shipping, etc)
- CFHT delivers the primary mirror and mirror support systems
- two options:
 - 1) refigure primary mirror maintaining conic constant and radius
 - maintain radius of curvature
 - maintain figure - parabola
 - 20 nm rms final figure error
 - test the delivered and in-process optical figure
 - 2) regrind/ refigure to a shorter focal length / new conic
 - radius change from 27 m to 15 m
 - 20 nm rms final figure error
 - test the delivered and in-process optical figure

Image quality improvement program (IQIP)

The Image Quality Improvement Program SAC / BoD – 2010
(a cost-effective means to improve CFHT's delivered image quality)

Four components:

- 1) Dome Venting – in process
- 2) Thermal Imbalance Mitigation - staffing
- 3) Dome Painting – LoMIT - after vent installation
- 4) Primary and Secondary Mirror Refiguring – ROM quotes

Primary mirror refiguring – ROM cost estimates

Company	Refigure	Regrind / refigure
Exelis (Kodak, ITT)	\$2400k US / 77 wks	No interest
L3 – Brashear (Contraves)	No interest	> \$3500k / 72 wks
LZOS (Moscow)	\$ 325k US / 36 wks	No response
Sagem (Paris)	\$1600k US / ?	> \$ 2890 US / ?
Uof Arizona mirror lab	Interest - No specifics	Interest - No specifics

IQIP - Thermal imbalance status

Kevin Ho, Karun Thanjuvar, Sarah Gadjadhar



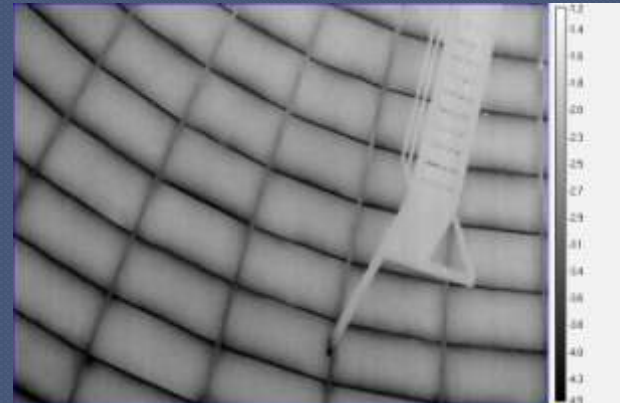
MegaCam storage electronics - SOLVED



Dome hydraulic motors - ELIMINATED



WIRCam (non) cooling - PENDING



Dome skin print through - VENTING